

RONDO-COANDA 125

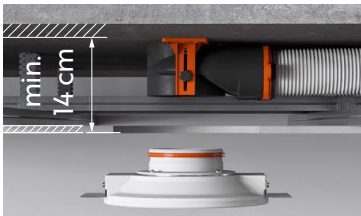
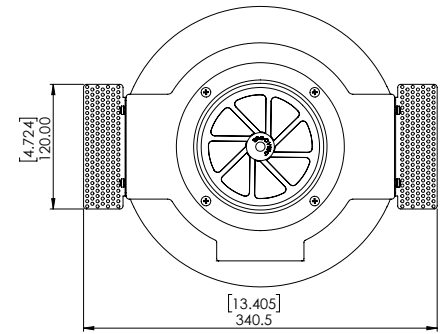
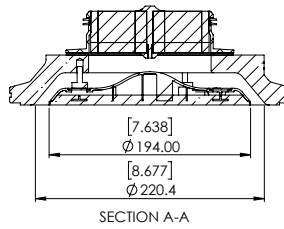
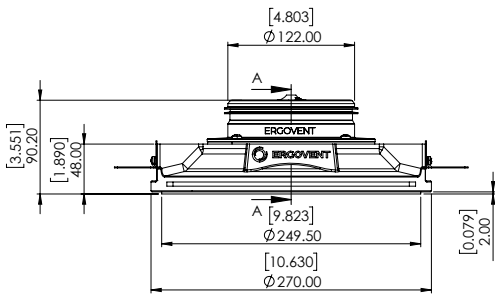
Hidden ventilation diffusers for ceilings and walls



The gypsum cover "armor" is a patented solution that protects against damage.

125mm connection / with damper

Round-shaped diffuser is a recessed ventilation diffuser designed to deliver air along the ceiling surface using the **COANDA effect** that is ideal for modern interiors where airflow comfort and discretion are key. Ideally suited for spaces where people are often directly beneath the diffuser—air movement is virtually imperceptible while the room's microclimate remains balanced. High-quality gypsum body: robust, bubble-free casting with integrated mounting elements. Smooth, paint-ready surface finish.



Minimum installation height: 140 mm ≈ 5,51"



A fiberglass liner is included with the product



Easy and fast installation

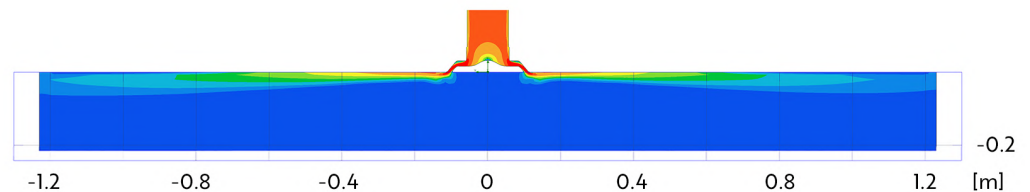


Airflow damper is included with the product

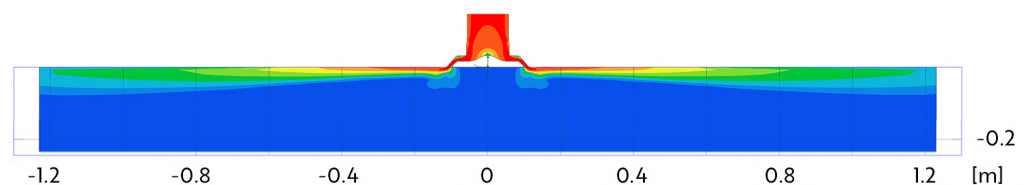
THROW DISTANCE



85 m³/h



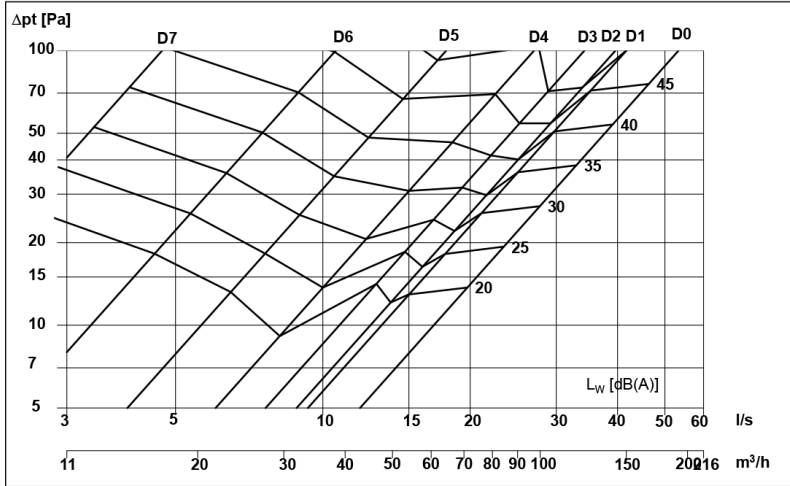
120 m³/h



FLOW NOISE (in accordance with ISO 3741) and PRESSURE DROP test report

SUPPLY

Diagram for pressure and flow noise:



$$L_{W_{oct}} [dB] = L_{WA} + K_{oct}$$

| q [l/s] | Dp _t [Pa] | L _{WA} [dBA] | | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1000 Hz | 2000 Hz | 4000 Hz | 8000 Hz |
|---------|----------------------|-----------------------|------------------|-------|--------|--------|--------|---------|---------|---------|---------|
| - | - | 33 | K _{oct} | -6 | 0 | -1 | -4 | -4 | -7 | -17 | -22 |

Octave correction factors to the diagram are calculated at the listed value of either q, Δp_t or L_{WA}/L_{DA}

Calculation of pressure and sound effect according to flow:

Sound effect: $L_{W(oct\ or\ A)} = k \cdot \log(q) + L_0$

L_W - sound effect [dB]

q - flow [l/s]

k - factor, sound effect [-]

K_{factor} - factor, balancing [l/(s·√Pa)]

Total pressuredrop: $\Delta p_t = c_{pt} \cdot q^2$

L₀ - addend, sound effect [-]

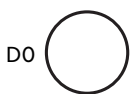
p_i - pressuredifference, balancing [Pa]

Δp_t - total pressuredrop [Pa]

Balancing: $q = K_{factor} \cdot \sqrt{p_i}$

c_{pt} - factor, total pressuredrop [Pa·s²/l²]

| | Total p c _{ptot} | Balancing K-factor | | L _{WA} | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1000 Hz | 2000 Hz | 4000 Hz | 8000 Hz |
|-----------|------------------------------|-----------------------|---------|-----------------|----------------|---------------|---------------|---------------|---------------|----------------|----------------|----------------|
| D0 | 0.0352 | Not measured | k Lo | 67.3 -67.2 | 50.8 -42.6 | 48.9 -32.8 | 70.9 -68.4 | 73.4 -79.2 | 65.9 -75.0 | 59.9 -65.4 | 69.4 -88.2 | 69.9 -92.8 |
| D1 | 0.0576 | Not measured | k Lo | 67.2 -59.0 | 72.5 -78.1 | 37.7 -16.4 | 51.8 -37.5 | 64.6 -57.7 | 63.7 -59.7 | 78.1 -81.5 | 81.4 -94.5 | 82.9 -104.4 |
| D2 | 0.0639 | Not measured | k Lo | 76.6 -67.2 | 86.8 -93.4 | 58.3 -43.3 | 52.4 -36.8 | 67.0 -59.2 | 78.3 -73.5 | 82.0 -80.3 | 90.2 -104.0 | 90.6 -110.8 |
| D3 | 0.0855 | Not measured | k Lo | 85.5 -74.8 | 86.1 -83.4 | 32.1 -6.6 | 58.9 -42.9 | 77.6 -70.4 | 87.0 -79.4 | 99.1 -100.8 | 87.2 -95.7 | 88.4 -102.0 |
| D4 | 0.1371 | Not measured | k Lo | 56.7 -31.7 | 58.4 -38.8 | 43.3 -19.8 | 51.4 -31.4 | 57.0 -39.9 | 56.8 -34.8 | 56.7 -37.3 | 74.6 -72.5 | 74.9 -76.7 |
| D5 | 0.3139 | Not measured | k Lo | 71.1 -37.7 | 63.4 -36.3 | 40.2 -5.1 | 75.5 -43.2 | 63.1 -34.0 | 70.2 -40.0 | 76.3 -51.4 | 71.8 -56.0 | 72.4 -62.0 |
| D6 | 0.8871 | Not measured | k Lo | 68.0 -24.6 | 24.5 10.9 | 24.0 13.2 | 61.2 -18.8 | 65.9 -25.9 | 63.7 -26.1 | 78.4 -40.7 | 73.4 -44.3 | 75.9 -51.1 |
| D7 | 4.5308 | Not measured | k Lo | 69.0 -6.7 | 101.4 -34.5 | 39.7 0.2 | 47.6 -1.0 | 59.2 -6.4 | 80.1 -17.1 | 61.3 -8.4 | 67.9 -18.2 | 68.5 -23.9 |



D0 no damper



D1 1 segment



D2 2 segments



D3 3 segments



D4 4 segments / full open



D5 4 segments / 75% open



D6 4 segments / 50% open

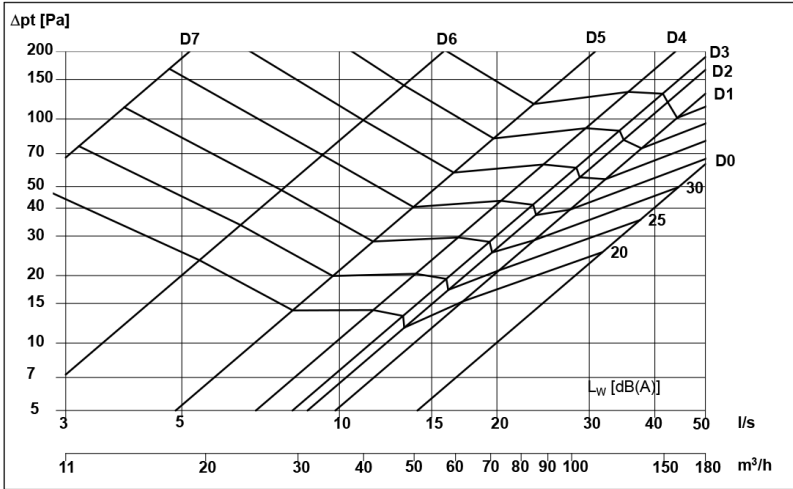


D7 4 segments / 25% open

FLOW NOISE (in accordance with ISO 3741) and PRESSURE DROP test report

EXTRACT

Diagram for pressure and flow noise:



$$L_{W_{oct}} [dB] = L_{WA} + K_{oct}$$

| q [l/s] | Δp _t [Pa] | L _{WA} [dBA] | | K _{oct} | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1000 Hz | 2000 Hz | 4000 Hz | 8000 Hz |
|---------|----------------------|-----------------------|--|------------------|-------|--------|--------|--------|---------|---------|---------|---------|
| - | - | 33 | | | 0 | -1 | -3 | -3 | -5 | -6 | -13 | -21 |

Octave correction factors to the diagram are calculated at the listed value of either q, Δp_t or L_{WA}/L_{DA}

Calculation of pressure and sound effect according to flow:

Sound effect: $L_{W(Oct \text{ or } A)} = k \cdot \log(q) + L_0$

L_W - sound effect [dB]

q - flow [l/s]

k - factor, sound effect [-]

K_{factor} - factor, balancing [l/(s·√Pa)]

Total pressuredrop: $\Delta p_t = c_{pt} \cdot q^2$

L₀ - addend, sound effect [-]

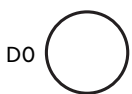
p_t - pressuredifference, balancing [Pa]

Δp_t - total pressuredrop [Pa]

Balancing: $q = K_{factor} \cdot \sqrt{p_t}$

c_{pt} - factor, total pressuredrop [Pa·s²/l²]

| | Total p c _{ptot} | Balancing K-factor | | L _{WA} | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1000 Hz | 2000 Hz | 4000 Hz | 8000 Hz |
|-----------|------------------------------|-----------------------|----|-----------------|-------|--------|--------|--------|---------|---------|---------|---------|
| D0 | 0.0252 | Not measured | k | 69.2 | 42.8 | 45.1 | 84.0 | 46.2 | 57.7 | 87.6 | 84.0 | 84.2 |
| | | | Lo | -83.9 | -35.8 | -39.2 | -113.1 | -49.7 | -69.5 | -121.2 | -122.1 | -128.4 |
| D1 | 0.0518 | Not measured | k | 73.4 | 26.5 | 53.8 | 52.7 | 48.2 | 67.7 | 83.5 | 84.8 | 85.4 |
| | | | Lo | -70.7 | -5.3 | -44.6 | -45.1 | -38.8 | -68.5 | -90.1 | -100.0 | -109.1 |
| D2 | 0.0662 | Not measured | k | 59.7 | 20.7 | 23.5 | 35.6 | 42.9 | 59.0 | 69.0 | 77.7 | 77.7 |
| | | | Lo | -47.1 | 6.6 | 1.6 | -17.0 | -27.3 | -51.5 | -66.0 | -84.5 | -92.7 |
| D3 | 0.0755 | Not measured | k | 60.5 | 56.9 | 56.0 | 61.3 | 49.6 | 62.9 | 61.9 | 71.2 | 72.2 |
| | | | Lo | -47.9 | -44.9 | -41.1 | -51.6 | -36.3 | -57.6 | -55.4 | -75.0 | -84.9 |
| D4 | 0.1042 | Not measured | k | 61.6 | 46.0 | 56.3 | 56.1 | 53.3 | 59.2 | 67.0 | 77.4 | 78.7 |
| | | | Lo | -45.5 | -30.1 | -39.3 | -39.8 | -37.6 | -48.1 | -58.9 | -80.1 | -89.5 |
| D5 | 0.2111 | Not measured | k | 65.1 | 85.0 | 46.8 | 58.0 | 58.1 | 60.4 | 73.9 | 88.8 | 89.9 |
| | | | Lo | -39.3 | -65.9 | -19.8 | -33.2 | -33.8 | -38.3 | -57.0 | -80.6 | -89.0 |
| D6 | 0.8025 | Not measured | k | 64.0 | 32.0 | 51.8 | 41.2 | 58.3 | 71.2 | 65.3 | 84.5 | 85.1 |
| | | | Lo | -26.9 | 2.8 | -18.1 | -6.4 | -24.1 | -39.3 | -35.1 | -59.8 | -67.9 |
| D7 | 7.4766 | 17.2 | k | 57.9 | 40.3 | 40.6 | 56.0 | 39.5 | 50.1 | 73.3 | 68.2 | 69.3 |
| | | | Lo | -4.1 | 11.2 | -1.7 | -11.0 | 3.1 | -3.1 | -20.3 | -23.1 | -28.8 |



no damper



1 segment



2 segments



3 segments



4 segments /
full open



4 segments /
75% open



4 segments /
50% open



4 segments /
25% open